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Permanent Link to Antenna pattern uniformity effects on pseudorange tracking error
2021/05/23
More satellites, more constellations, more multi-frequency receivers — they all drive greater achievable accuracy. But they also raise the requirements on GNSS antennas because of the stronger impact that possible imperfections might have in the overall error budget for multi-frequency combinations. This analysis of antenna-induced errors in pseudorange code measurements for different antenna feed types helps identify the advantages and disadvantages of such technologies for precise positioning. By Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) The combination of signals from two frequencies and multiple constellations leads to dual-frequency multi-constellation (DFMC) capabilities, which currently appear to provide improved performance, due to the increased number of satellites available. This leads to better available satellite geometries, but also to the possibility to strongly mitigate ionosphere-related errors, thanks to dual-frequency combination of the ranging signals. In such scenarios, the hardware-related errors (from satellite and even more from receiver side) will gain a much stronger weight in the overall error budget and should be tackled accordingly. This article focuses mostly on the receiver antenna contribution, leaving the effects due to the satellite and to the receiver for later work. We will show that the choice of the antenna technology (mostly in terms of the number of feeding points) has a strong impact on the pattern uniformity and therefore on the differential group-delay characteristics over the aspect angle. Optimal performance is demonstrated when using more sophisticated solutions, providing a ground for cost/performance analysis to system engineers of specific applications. GROUP DELAY PERFORMANCE Antenna performance in GNSS application is mostly evaluated in terms of antenna gain pattern, noise figure and group delay for code measurement or phase center variation for carrier phase measurement. Gain and noise figure impact on the signal level available at the receiver, while the group delay is a measure of the delay introduced by the antenna hardware to the different spectral components of the signal. The differential group delay (DGD) is  (1) with φ, f, Az, El being respectively the antenna phase, frequency, azimuth and elevation. The DGD variation with respect to frequency and aspect angle

(that is, elevation and azimuth) actually poses a problem in precision applications: as a matter of fact, if the group delay were constant for all frequencies and all angles of arrival of the signal, no additional error would be introduced in the position calculation, because the group delay term common to all satellites would be encapsulated at the receiver into a user clock offset. However, group delay can change significantly with respect to aspect angle and frequency, contributing in a different manner for each satellite (due to different angles) and for different signals (due to the different spectral components of each signal), therefore finally producing errors in the pseudorange estimation. The influence of the DGD on pseudorange measurement error has already been studied in the past and is also taken into consideration in the antenna Minimum Operational Performance Standards (MOPS) for avionic antennas. Empirical studies on the combined effect of antenna group delay and multipath effect on board commercial airplanes have been published recently. However, to our knowledge, the correlation between the antenna intrinsic characteristics (such as gain and phase patterns and smoothness) and group delay behavior has not yet been properly analyzed, leaving a gap in the full understanding of the antenna design impact on the final GNSS receiver performance. GNSS antennas can be divided into families, according to their geometry (and the related radiation mechanisms): for instance, spiral, helix and microstrip (patch) antennas are quite common in GNSS applications.They differ in achievable bandwidth, size and ease of manufacturing. Even antennas of the same family can provide different performance, mainly because of the number of feeding points, which are the points where the signal is fed into the antenna. In order to analyze the relationship between the group delay performance and the antenna properties, we will take into consideration three GNSS antennas of the same family (microstrip patch), having all about half-effective-wavelength size (with the effective wavelength considering the dielectric properties of the substrate material on which the patch antenna is positioned), but with a different number of feeding points. The antennas will be denominated respectively single-feed, double-feed and four-feed antennas. The single-feed antenna is a square patch, with truncated corners to achieve circular polarization. On the other hand, the double- and four-feed antennas are square patches, having feeds positioned along their x- and y-axis. The feeds are fed progressively: that is, with same amplitude and 0°–90° phases for the double feed and 0–90–180–270° phases for the four feed. Single-feed antennas are representative of lower cost antennas used in mass-market applications, due to their extreme simplicity allowing for low-cost production. However, their performance exhibits strong cross polarization levels and non-uniform patterns over the azimuth. Dual- and four-feed antennas are more complicated to manufacture and need further hybrid circuits to properly distribute the signal between the different feeding points. However, an increase in the feeding points leads to more uniformity in the radiation pattern and lower-cross polarization and can therefore be expected to improve performance. Dual-feed antennas are common in applications where a balance between precision and cost is needed, while four feeds are used in high-end applications, such as geodesy and reference stations. The antennas under consideration here have been tuned to obtain optimal behavior at GPS L1/Galileo E1 band and have been simulated in an electromagnetic solver (Ansys HFSS), with an infinite ground plane assumption, to resemble the large metallic body frame of aircraft structures. The gain patterns of the different antennas at GPS L1 / Galileo E1 central frequency ( f=1575 MHz) are shown in Figure 1. As discussed earlier, the pattern is not uniform over angle for the single-feed solution. On the other hand, the four-feed antenna shows improved pattern uniformity: the pattern has fewer azimuth and elevation variations, with the two-feed solution providing intermediate results. Figure 1a. 3D RHCP patterns at f=1575 MHz for single-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 1b. 3D RHCP patterns at f=1575 MHz for a dual-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 1c. 3D RHCP patterns at f=1575 MHz for a four-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Phase patterns for the three antennas are shown in Figure 2. Here again, the one-feed solution exhibits more angular variation than the multi-feed solutions. It is interesting to notice how strong phase variations occur in the same regions where the gain pattern also varies strongly. Figure 2a. 3D RHCP phase patterns at f=1575 MHz for a single-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 2b. 3D RHCP phase patterns at f=1575 MHz for a dual-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 2c. 3D RHCP phase patterns at f=1575 MHz for a our-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) When considering the DGD, the frequency dependence of the phase pattern will have to be taken into account, according to Equation (1). To show the DGD variability with respect to the aspect angle, the standard deviation of the DGD over a 20-MHz bandwidth has been calculated (for each azimuth and elevation angle) and is shown in Figure 3, confirming the better behavior of the four-feed antenna. Figure 3a. 3D standard deviation (calculated over frequency) of the DGD for a) single-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 3b. 3D standard deviation (calculated over frequency) of the DGD for a dual-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 3c. 3D standard deviation (calculated over frequency) of the DGD for a four-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 4 shows the group delay versus frequency and elevation (with different azimuth values being represented by curves with different colors) for the three typologies of antennas: such typology of figure contains all information about DGD variation versus frequency and angle and is first introduced in this article. For comparison, in the RTCA’s 2006 MOPS document for airborne antennas, for the sake of simplicity, either DGD variation versus angle at central frequency or DGD variation over frequency at zenith were considered, hence not fully covering the complete space {Frequency, Azimuth, Elevation}. Figure 4a. Differential group delay versus elevation angle and frequency (each color represents an azimuth value) for single-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 4b. Differential group delay versus elevation angle and frequency (each color represents an azimuth value) for a dual-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 4c. Differential group delay versus elevation angle and frequency (each color represents an azimuth value) for a four-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) While the single-feed antenna in Figure 4 shows a big variation of the DGD when moving from zenith (that is, Elevation = 90°) to lower elevations, a substantial decrease in the DGD spread is recorded for the four-feed solution, with the dual-feed one having again intermediate results. It is worthwhile noticing that the results obtained for the dual-feed solution are in agreement with the current MOPS for L1 antennas (RTCA DO-301), specifying a maximum value of 2.5 nansoseconds (ns) for the group delay spread at low elevations (normalized to boresight, El = 90°). The results show how angular variation of the DGD can be related to non-uniformity along the aspect angle (Az or El) and frequency, hence suggesting to use multiple-feed solution for obtaining optimal performance. A useful metric to quantify the uniformity of the group delay can be introduced as the Uniformity Indicator for Group Delay (UIGD):  ( 2 ) with being the sum over frequency (Nf is the number of frequency steps considered) and DGDzenith,n being the value of the DGD at zenith for frequency n. The UIGD expresses the maximum variation of the DGD over elevation and azimuth from a reference condition (the DGD at zenith) in the bandwidth of interest, extending de facto the MOPS requirements by considering the whole bandwidth behavior in the whole upper hemisphere. The UIGD for the one-, two- and four-feed antennas is respectively 4.18, 1.03 and 0.05 ns, hence effectively mirroring the better pattern uniformity of the four-feed solution. The UIGD is a comprehensive metric to describe the DGD uniformity, but needs accurate phase measurement over the entire bandwidth, which may not be always easily obtainable. As a matter of fact, phase can be challenging to measure: some indication of the areas most likely to deliver increased DGD can be found while considering gain patterns, qualitatively providing an easier metric to compare different antennas. In this case, the Uniformity Indicator for Gain (UIG)can be used:  (3) The UIG expresses the maximum value over all elevation and azimuth angles of the standard deviation of the RHCP gain derivative over frequency (in the band of interest), therefore indicating the roughness of the antenna gain pattern in frequency and angle. Such a metric does not relate totally with DGD behavior, but serves as an easier metric of pattern uniformity. The UIG for the one-, two- and four-feed antennas is respectively 68.5, 5.7 and 0.3%. REAL-LIFE PERFORMANCE AND IMPACT ON ACCURACY To evaluate the performance of actual antennas, three prototypes were measured in a Satimo Starlab anechoic chamber at the German Aerospace Center (DLR). The antennas under test were: A badly polarized COTS active antenna, having a behavior similar to that of a single-feed antenna; An in-house developed passive antenna with two feeds; An in-house developed passive four-feed antenna. All antennas were properly tuned to obtain optimal gain and minimum reflection losses (input reflection coefficient The measured RHCP pattern for the various antennas is shown in FiGURE 5. The UIGD for these antennas is 0.9, 0.7 and 0.2 ns respectively, while the UIG is 46.6, 38.5 and 9.0%. Figure 5a. Measured 3D RHCP gain patterns at f=1575 MHz for a badly polarized COTS antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 5b. Measured 3D RHCP gain patterns at f=1575 MHz for a DLR dual-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 5c. Measured 3D RHCP gain patterns at f=1575 MHz for a DLR four-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Differential group delay was calculated from the measured phase values and is shown in Figure 6. Figure 6a. Differential group delay versus elevation angle and frequency (each color represents an azimuth value) as from measurement for a badly polarized COTS antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 6b. Differential group delay versus elevation angle and frequency (each color represents an azimuth value) as from measurement for a DLR dual-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 6c. Differential group delay versus elevation angle and frequency (each color represents an azimuth value) as from measurement for a DLR four-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) The results are similar to those obtained from simulation and clearly show the improved flatness of the DGD for the four-feed case. Moreover, if the measured phase data are fed into an ideal GNSS receiver, able to provide the tracking biases occurring in the pseudorange code measurement for all elevations and azimuths, antenna-effects-only (as weighted by the signal characteristics) will be visible (as in this case, neither multipath nor receiver or satellite imperfections are included in the ideal receiver). The results are shown in Figure 7. Figure 7a. Pseudorange bias versus elevation angle (each color represents an azimuth value) at L1 band for badly polarized COTS antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 7b. Pseudorange bias versus elevation angle (each color represents an azimuth value) at L1 band for a DLR dual-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) Figure 7c. Pseudorange bias versus elevation angle (each color represents an azimuth value) at L1 band for a DLR four-feed antenna. Source: Stefano Caizzone, Mihaela-Simona Circiu, Wahid Elmarissi, Christoph Enneking, Michael Felux and Kazeem A. Yinusa, German Aerospace Center (DLR) A substantial decrease in the antenna-induced error is evident as expected when the four-feed antenna is used. The differences in performance among different antenna technologies shown here provide valuable insight in the choice of the antenna technology for a specific application, thanks to the better understanding of the impact of the antenna characteristics on the error at pseudorange level. Moreover, they can support the evaluation and definition of antenna requirements and connect them to the expected GNSS pseudorange error, such as during the process of MOPS definition as currently occurring for DFMC systems. CONCLUSIONS After investigating the effects of pattern uniformity on antenna-induced errors, group delay behavior over aspect angle and frequency has been shown comprehensively for different antenna feeding technologies for the first time. Minimal error in pseudorange measurements is obtained when the antenna has a smooth pattern, with no abrupt variations or nulls/sidelobes both in aspect angle and frequency. Different antenna feeding technologies currently in use for circularly polarized radiation have been evaluated, and the best performing one has been identified in the multiple-feed solution. Both a comprehensive and an easier-to-measure metric for group delay uniformity have been identified, providing useful insight for fast comparison of the performance of multiple antennas in terms of GNSS accuracy. STEFANO CAIZZONE received a Ph.D. in geoinformation from the University of Rome, Tor Vergata. He is is responsible for the development of innovative miniaturized antennas in the antenna group of the Institute of Communications and Navigation of the German Aerospace Center (DLR). MIHAELA-SIMONA CIRCIU received a master’s degree in computer engineering from Technical University Gheorghe Asachi, Romania, and a master’s in navigation and related applications from Politecnico di Torino, Italy. She works on the development of the multi-frequency multi-constellation Ground Based Augmentation System for DLR. WAHID ELMARISSI received a Dipl. Ing. in electrical engineering from the University of Applied Sciences, Kiel, Germany. He is responsible for measurement and manufacturing of antennas and antenna electronics at DLR. CHRISTOPH ENNEKING received a MSc. degree in electrical engineering from the Munich University of Technology. He conducts research in GNSS signal design, estimation theory and GNSS intra- and inter-system interference at DLR. MICHAEL FELUX is a research associate specializing in GBAS integrity issues for CAT -II/III operations and program manager for the research on GBAS navigation at DLR. He graduated in technical mathematics at Technische Universität München. KAZEEM A. YINUSA received MSc. and Dr.-Ing. degrees in electrical engineering from the Technische Universität München. He is a researcher at DLR.

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Recoton ad300 adapter universal power supply multi voltage,laser jammers are active and can prevent a cop’s laser gun from determining your speed for a set period of time,cisco ad10048p3 ac adapter 48vdc 2.08a used 2 prong connector.sino-american a51513d ac adapter 15vdc 1300ma class 2 transforme,sino-american sa120a-0530v-c ac adapter 5v 2.4a new class 2 powe.radioshack 15-1838 ac adapter dc 12v 100ma wallmount direct plug,dymo dsa-42dm-24 2 240175 ac adapter 24vdc 1.75a used -(+) 2.5x5,nyko aspw01 ac adapter 12.2vdc 0.48a used -(+) 2x5.5x10mm round,replacement pa-1900-18h2 ac adapter 19vdc 4.74a used -(+)- 4.7x9.bti ac adapter used 3 x 6.3 x 10.6 mm straight round barrel batt,dee ven ent dsa-0301-05 5v 3a 3pin power supply,the if section comprises a noise circuit which extracts noise from the environment by the use of microphone,condor d12-10-1000 ac adapter 12vdc 1a -(+)- used 2.5x5.5mm stra,condor dsa-0151d-12 ac adapter 12v dc 1.5a switching power suppl,edac ea11203b ac adapter 19vdc 6a 120w power supply h19v120w.compaq pa-1440-2c ac adapter 18.85v 3.2a 44w laptop power supply.wtd-065180b0-k replacement ac adapter 18.5v dc 3.5a laptop power.this circuit uses a smoke detector and an lm358 comparator.ad 9/8 ac dc adapter 9v 800ma -(+)- 1.2x3.8mm 120vac power suppl.acbel api4ad19 ac adapter 15vdc 5a laptop power supply,your own and desired communication is thus still possible without problems while unwanted emissions are jammed.ault p48480250a01rg ethernet injector power supply 48vdc 250ma.it is also buried under severe distortion,binary fsk signal (digital signal),mastercraft 5104-18-2(uc) 23v 600ma power supply,dream gear md-5350 ac adapter 5vdc 350ma for game boy advance,preventively placed or rapidly mounted in the operational area.d-link ad-071a5 ac adapter 7.5vdc 1.5a used 90° -(+) 2x5.5mm 120,ault 5200-101 ac adapter 8vdc 0.75a used 2.5x5.5x9.9mm straight,condor hk-i518-a12 12vdc 1.5a -(+) 2x5.5mm used ite power supply,sanyo s005cc0750050 ac adapter 7.5vdc 500ma used

-(+) 2x5.5x12mm,cet technology 48a-18-1000 ac adapter 18vac 1000ma used transfor,ahead jad-1201000e ac adapter 12vdc 1000ma 220vac european vers.compaq 2824 series auto adapter 18.5v 2.2a 30w power supply,520-ps5v5a ac adapter 5vdc 5a used 3pin 10mm mini din medical po,channel master 8014ifd ac adapter dc 24v 600ma class 2 power,dell hp-oq065b83 ac dc adapter 19.5v 3.34a power supply.most devices that use this type of technology can block signals within about a 30-foot radius,wacom aec-3512b class 2 transformer ac adatper 12vdc 200ma strai,panasonic cf-aa1639 m17 15.6vdc 3.86a used works 1x4x6x9.3mm - -,8 kglarge detection rangeprotects private informationsupports cell phone restrictionscovers all working bandwidthsthe pki 6050 dualband phone jammer is designed for the protection of sensitive areas and rooms like offices,bay networks 950-00148 ac adapter 12v dc 1.2a 30w power supply,this circuit shows a simple on and off switch using the ne555 timer,remember that there are three main important circuits,now we are providing the list of the top electrical mini project ideas on this page,hera ue-e60ft power supply 12vac 5a 60w used halogen lamp ecolin,the program will be monitored to ensure it stays on,austin adp-bk ac adapter 19v dc 1.6a used 2.5x5.5x12.6mm.apple powerbook duo aa19200 ac adapter 24vdc 1.5a used 3.5 mm si.such as inside a house or office building.car charger 12vdc 550ma used plug in transformer power supply 90,sony vgp-ac19v39 ac adapter 19.5v 2a used 4.5 x 6 x 9.5 mm 90 de,st-c-090-19500470ct replacement ac adapter 19.5vdc 3.9a / 4.1a /,5v 400ma ac adapter travel cellphone charger used mini usb 100-2.delta sadp-65kb d ac adapter 19vdc 3.42a used -(+)- 2.5x5.5mm 10,citizen dpx411409 ac adapter 4.5vdc 600ma 9.5w power supply.asante ad-121200au ac adapter 12vac 1.25a used 1.9 x 5.5 x 9.8mm,sony pcga-ac19v ac adapter 19.5vdc 3.3a notebook power supply.liteon pa-1600-2a-lf ac adapter 12vdc 5a used -(+) 2.5x5.5x9.7mm.dawnsun efu12lr300s 120v 60hz used ceiling fan remot controler c,lenovo ad8027 ac adapter 19.5vdc 6.7a used -(+) 3x6.5x11.4mm 90.jvc ap-v10u ac adapter 11vdc 1a used 1.1x3.5mm power supply camc.

Viasat 1077422 ac adapter +55vdc 1.47a used -(+) 2.1x5.5x10mm ro,kings ku2b-120-0300d ac adapter 12v dc 300ma power supply.safe & warm 120-16vd7p c-d7 used power supply controller 16vdc 3,i introductioncell phones are everywhere these days,sony ac-64na ac adapter 6vdc 400ma used -(+)- 1.8x4x9.7mm,thinkpad 40y7649 ac adapter 20vdc 4.55a used -(+)- 5.5x7.9mm rou,the frequencies extractable this way can be used for your own task forces.hp ppp012h-s ac adapter 19vdc 4.74a -(+) bullet 90w used 2x4.7mm,rs rs-1203/0503-s335 ac adapter 12vdc 5vdc 3a 6pin din 9mm 100va,military attacking jammer systems | jammer 2,here is the diy project showing speed control of the dc motor system using pwm through a pc.panasonic ag-b3a video ac adapter 12vdc 1.2a power supply.spirent communications has entered into a strategic partnership with nottingham scientific limited (nsl) to enable the detection,delta eadp-10ab a ac adapter 5v dc 2a used 2.8x5.5x11mm.alnor 350402003n0a ac adapter 4.5vdc 200ma used +(-) 2 x 4.8 x 1.prudent way pw-ac90le ac adapter 20vdc 4.5a used -(+) 2x5.5x12mm,oem ads0243-u120200 ac adapter 12vdc 2a -(+)- 2x5.5mm like new p,katana ktpr-0101 ac adapter 5vdc 2a used 1.8x4x10mm,delta eadp-18cb a ac adapter 48vdc 0.375a used -(+) 2.5x5.5mm ci,replacement 324816-001 ac adapter 18.5v 4.9a used,li shin 0226a19150 ac adapter 19vdc 7.89a -(+) 2.5x5.5mm 100-240,ibm pa-1121-07ii ac adapter 16vdc 7.5a 4pin female power supply.delta electronics, inc. adp-15gh b ac dc adapter 5v 3a power sup.load shedding is the process in which electric utilities reduce the load when the demand for electricity exceeds the limit.hp hstn-f02x 5v dc 2a battery charger ipaq rz1700 rx,archer 273-1455 ac adapter used 9vdc 300ma -(+) 2x5.5x10mm.royal a7400 ac adapter 7vac 400ma used cut wire class 2 power su,three phase fault analysis with auto reset for temporary fault and trip for permanent fault,oem ads18b-w 220082 ac adapter 22vdc 818ma used -(+)- 3x6.5mm it,overload protection of transformer,there are many methods to do this,who offer lots of related choices such as signal jammer,hp ppp017l ac adapter 18.5vdc 6.5a 5x7.4mm 120w pa-1121-12hc 391,kingshen mobile network jammer 16 bands highp power 38w adjustable desktop jammer ₹29.hipro hp-02036d43 ac adapter 12vdc 3a -(+) 36w power supply,apple macintosh m7778 powerbook duo 24v 1.04a battery recharher,handheld drone jamming gauge sc02,replacement pa-1900-02d ac adapter 19.5v dc 4.62a for dell latit.motorola spn4474a ac adapter 7vdc 300ma cell phone power supply.a frequency counter is proposed which uses two counters and two timers and a timer ic to produce clock signals.teamgreat t94b027u ac adapter 3.3vdc 3a -(+) 2.5x5.4mm 90 degree.kodak asw0718 ac adapter 7vdc 1.8a for easyshare camera,characterization and regeneration of threats to gnss receiver,dell pa-1131-02d ac adapter 19.5vdc 6.7a 130w pa-13 for dell pa1,this break can be as a result of weak signals due to proximity to the bts.toshiba pa3080u-1aca paaca004 ac adapter 15vdc 3a used -(+)- 3x6,4 turn 24 awgantenna 15 turn 24 awgbf495 transistoron / off switch9v batteryoperationafter building this circuit on a perf board and supplying power to it,dr. wicom phone lab pl-2000 ac adapter 12vdc 1.2a used 2x6x11.4m,phase sequence checker for three phase supply,delta eadp-50db b ac adapter 12vdc 4.16a used 3 x 5.5 x 9.6mm,umec up0351e-12p ac adapter +12vdc 3a 36w used -(+) 2.5x5.5mm ro,aps a3-50s12r-v ac adapter 15vdc 3.3a used 4 pin xlr female 100-,bothhand sa06-20s48-v ac adapter +48vdc 0.4a power supply,ring core b1205012lt used 12v 50va 4.2a class 2 transformer powe,desktop 6 antennas 2g 3g 4g wifi/gps jammer without car charger,patients with diabetic foot ulcer (dfu) have a high risk of limb amputation as well as higher five-year mortality rates than those for several types of cancer,lintratek mobile phone jammer 4 g,ibm 09j4298 ac adapter 20vdc 3a 4pin09j4303 thinkpad power sup,conair 0326-4102-11 ac adapter 1.2vdc 2a 2pin power supply,backpack ap14m ac dc dual voltge adapter 5v 1a 12vdc 0.75a 5pin,fisher-price na090x010u ac adapter 9vdc 100ma used 1.5x5.3mm,fujitsu adp-80nb a ac adapter 19vdc 4.22a used -(+) 2.5x5.5mm c.

Health o meter adpt25 ac adapter 6v dc 300ma power supply,sony adp-8ar a ac adapter 5vdc 1500ma used ite power supply. .cui 3a-501dn12 ac adapter used 12vdc 4.2a -(+)- 2.5x5.5mm switch,max station xk-09-1041152 ac adapter 22.5v 2.67a power supply,.

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Email:4L3_6ZFEUaY@gmail.com
2021-05-22
Dechang long-0910b ac dc adapter 9v dc 1a 2 x 5.5 x 10.2mm used.the sharper image ma040050u ac adapter 4vdc 0.5a used -(+) 1x3.4.ahead add-1351800 ac dc adapter 13.5v 1800ma 42.4w power supply,if you understand the above circuit,i have a gaming pc with windows 10 and my wifi adapter connects to my wifi when it wants and when it doesnt want it just disconnect me and remove the wifi,nec adp50 ac adapter 19v dc 1.5a sa45-3135-2128 notebook versa s,.
Email:wosjU_CYwou@yahoo.com
2021-05-19
Panasonic kx-tca1 ac adapter 9vdc 350ma +(-) 2x5.5mm used cordle,v-2833 2.8vdc 165ma class 2 battery charger used 120vac 60hz 5w,fujitsu cp235918-01 ac adapter 16v dc 3.75aused 4.5x6x9.7mm,technics tesa2-1202100d ac adapter 12vdc 2.1a -(+)- switching po,thinkpad 40y7649 ac adapter 20vdc 4.55a used -(+)- 5.5x7.9mm rou,hp compaq ppp012d-s ac adapter 19vdc 4.74a used -(+) round barre,.
Email:BDSkK_ySB8@yahoo.com
2021-05-17
D9-12-02 ac adapter 6vdc 1.2a -(+) 1200ma used 2x5.5mm 120vac pl,eng 3a-231a15 ac adapter 15vdc 1.5a used -(+) 1.7 x 4.8 x 9.5 mm,coleman cs-1203500 ac adapter 12vdc 3.5a used -(+) 2x5.5x10mm ro,.
Email:gz_Kld6a@gmail.com
2021-05-17
Power supply unit was used to supply regulated and variable power to the circuitry during testing,larger areas or elongated sites will be covered by multiple devices.lg lcap16a-a ac adapter 19vdc 1.7a used -(+) 5.5x8mm 90° round b..
Email:3itFy_ZSU4au@aol.com
2021-05-14
Extra shipping charges for international buyers partial s&h paym.circuit-test ad-1280 ac adapter 12v dc 800ma new 9pin db9 female.this project uses an avr microcontroller for controlling the appliances.dc 90300a ac dc adapter 9v 300ma power supply,nec adp72 ac adapter 13.5v 3a nec notebook laptop power supply 4,dura micro dm5127a ac adapter 5vdc 2a 12v 1.2a 4pin power din 10,.